

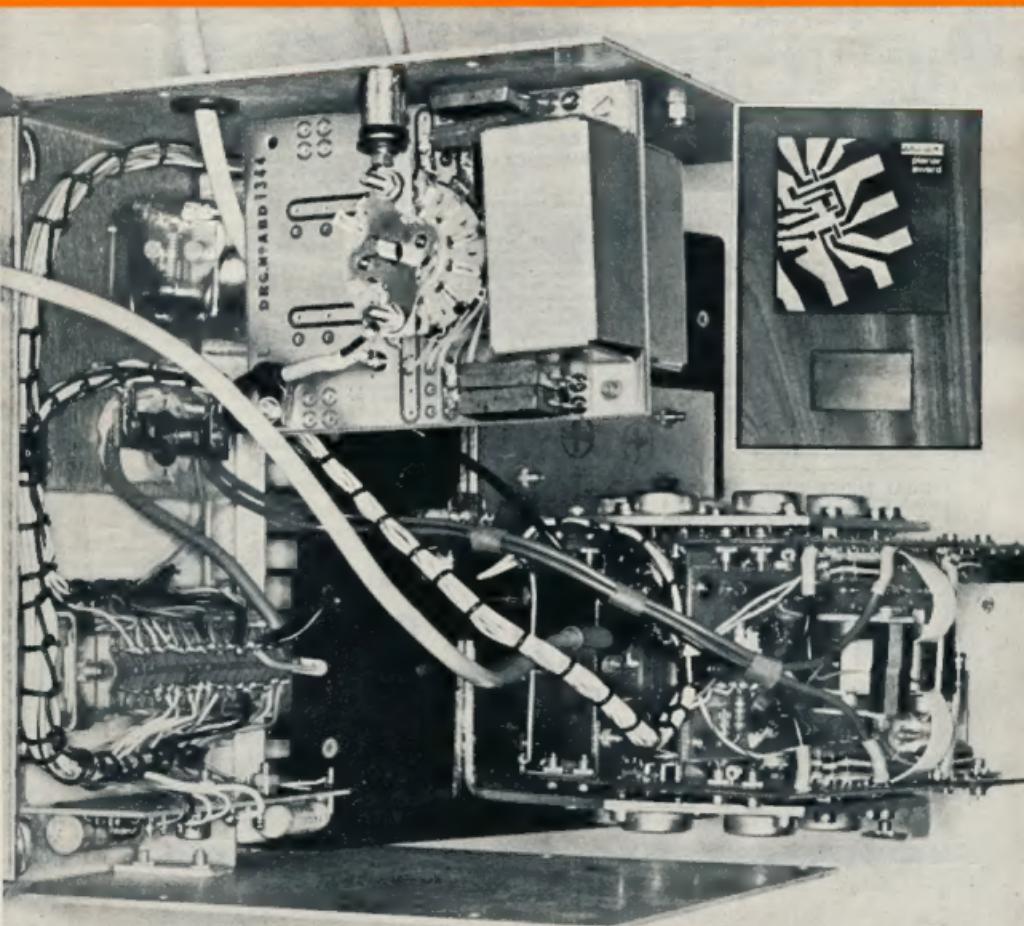
# amateur radio

Vol. 38, No. 12

DECEMBER, 1970

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# amateur radio

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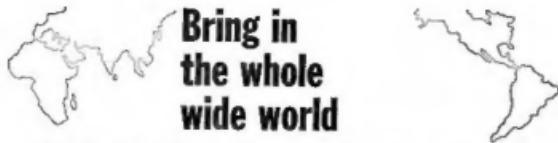
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## COVER STORY

Our front cover this month shows what is claimed to be the first commercially available, fully solid state, 100 watt linear high frequency amplifier in the world. The unit, manufactured by Racal (Aust.) Pty. Ltd., won the Fairchild Planar Award for 1970. Full story on page 18.



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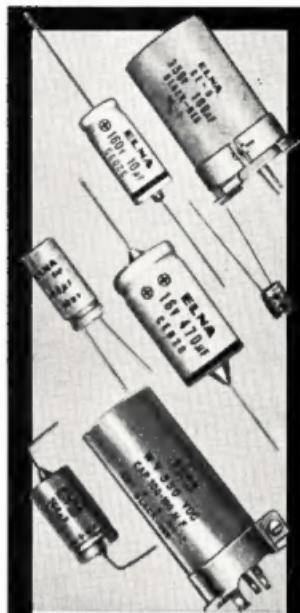
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## AN IMPORTANT SPEECH

The Annual Dinner of the Wireless Institute of Australia, Victorian Division, was held on Wednesday, 28th October. Amongst the guests were Mr. E. J. Wilkinson, Assistant Director-General Radio, and Mr. H. Young, Controller, Radio Branch. Also present was Mr. Bob Booth, W3PS, the General Counsel of the American Radio Relay League.

The toast to the Institute was proposed by Mr. Wilkinson and his speech in proposing the toast is of general interest. Mr. Wilkinson commenced by referring to the fact that this was the sixtieth year of the Wireless Institute. He pointed out that 1970 was significant for other reasons. Firstly, Australis Oscar-5 had been launched in 1970 which he described as probably the most meritorious effort in the history of the technical side of the Wireless Institute. He congratulated those concerned on their achievement and wished them "Good luck with the next one."

Mr. Wilkinson also pointed out that 1970 is the year of the skirmishing and behind-the-scenes lobbying in preparation for the 1971 World Administrative Radio Conference on Space Communications. He said that the Wireless Institute of Australia is in the front rank fighting for Amateurs' rights, seeking new spectrum above 20 GHz. and protecting its "real estate" below that frequency. Significantly, Mr. Wilkinson said that he believed that the Institute is holding its own—"Its performance to date certainly measures up with the other efforts in this area that we have seen from the Australian Post Office side."

He said that the Australian Post Office was conferring with the various users of radio frequency and many of these would jump at some of the precious areas that are at present allocated to the Amateur Service. Mr. Wilkinson

said, quite bluntly, that one of the pressures on the Post Office was the claim by these other users that the Amateur Service was not using its allocations. Once again I quote from what Mr. Wilkinson said:

"We know you're doing your best to hold on to the areas that you already have and enjoy—would you please help by making use of them! You may have seen some of the statements about the number of signals on the air in the 144 MHz. band and the 432 MHz. band. If ever there was a time for the Australian Amateur to make plenty of use of these v.h.f. low u.h.f. and even the higher u.h.f. bands that adjoin some of the areas that are being used by the space people, then this is the year and this is the time."

Then Mr. Wilkinson referred to a matter that is of far reaching significance in Amateur circles. I propose again to quote his words, but before doing so, this matter requires some little explanation. The allocation 7-7.1 MHz. is allocated on a world-wide basis exclusively to the Amateur Service. In Region III. and Region I., the band 7.1-7.3 MHz. is allocated to the broadcasting service. In Region II. that area is allocated exclusively to the Amateur Service. Early this year the Institute made representations to our Administration to extend the Australian Amateur allocation (which is 7-7.1 MHz. exclusive and 7.1-7.15 MHz. shared) to 7.3 MHz., thus bringing our allocation in line with the allocations in the United States of America and other Region II. countries.

In the course of his speech, Mr. Wilkinson made the first public reference to this representation: "Dare I mention the 7 MHz. band which will probably be dear to a few people's hearts. It is perhaps strange that at

the time that the space frequencies are being talked about, there is a strong feeling in the Australian Post Office that we ought to do something about bringing Australia into line with Region II. in that precious 7.1-7.3 MHz. area. Let's hope we can do something. You know it's a Region III. problem, not just Australia, but it might be some comfort for you to know that the Australian Post Office at least is hoping that it can swing this deal and help you to get back on an equal footing with Region II."

No doubt Mr. Wilkinson's comments are guarded in the extreme. Personally, I attach great significance to them and I hope that we may look forward to a time in the not too distant future when the Australian Amateur Service is able to use the 40 metre band up to 7.3 MHz.

Mr. Wilkinson concluded by congratulating the office-bearers of the Wireless Institute of Australia. He said that it was a great help to the Post Office to be able to deal with a united body—a group of people who they know represent the interests of the whole Amateur fraternity. He said that it would be a hopeless situation if they had to try and deal with individuals or with groups who were not as united as the Wireless Institute is. He said: "It's a credit to the members and to the office-bearers that we are able to get well reasoned and well represented cases and discuss them frankly and openly and come to what we believe to be a reasonable decision."

I know that Mr. Wilkinson regarded what he said in his speech as being of special significance. It is because I share that view that I have taken the unusual course of quoting from his speech at some length.

—MICHAEL OWEN, VK3KI,  
Federal President

# VK3 V.H.F. GROUP V.H.F. PRE-AMPLIFIER, MARK II.

This article has been essentially published to inform interested Amateurs of the changes in design and construction of the very successful v.h.f. pre-amplifier that originally appeared in "Amateur Radio" of July 1969. A great many enthusiasts have constructed this simple unit for operation within the Amateur bands, and more than a handful have been used in mobile radios by establishments outside the Amateur sphere of interest.

In response to suggestions by some interested Amateurs, we have undertaken to modify the old circuit and to include these in the new design. The suggestions were mainly concerned with protection of the semiconductor, however, as this required a change in the printed circuit design, we decided to examine the possibilities of further changes. By substituting a TIS88/2N5245 in place of the device originally used, we have now brought this unit into line with our two metre and 70 centimetre converters.

This device (TIS88) has been found to be totally reliable and exhibits more than enough desirable characteristics. Further, this would reduce the need to carry a wide range of semiconductor devices that essentially do the same operation.

Throughout these modifications, we have kept in the foreground of our consideration the basic requirements for the effort necessary in making changes mentioned above.

The design objectives of the pre-amplifier were:

- Best noise figure possible consistent with reasonable cost.
- Sufficient gain so that the system noise figure is determined by the pre-amplifier.

## PERFORMANCE

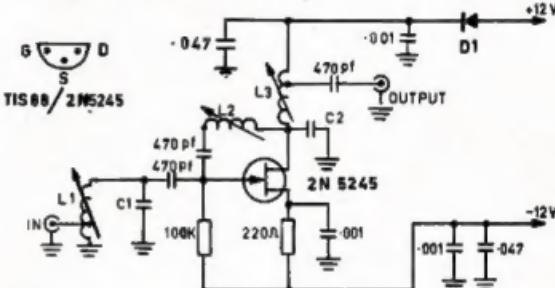
Once again noise figures of better than 2dB. have been obtained on both 2 and 6 metres. The gain on 2 metres is usually in excess of 18 dB, with gains of 22 dB. quite common. The gain on 6 metres, although not accurately measured, would as a function of the device parameters be slightly more.

## DESCRIPTION

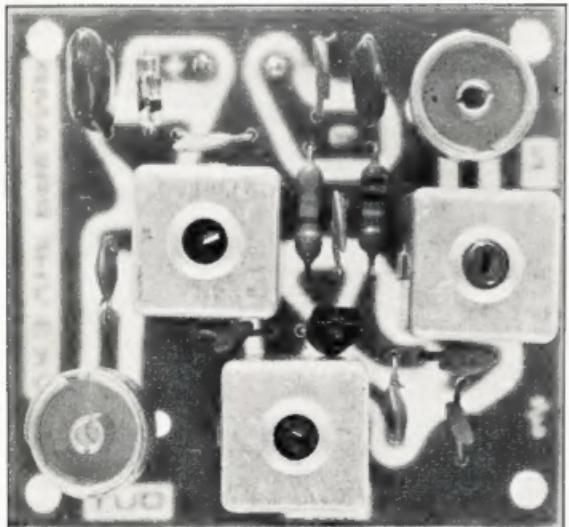
The pre-amplifier uses an TIS88/2N5245 JFET (Texas) in neutralised

common source configuration. Neutralisation is accomplished by adjustment of L2, which resonates with the drain to gate feedback capacitance to form a high impedance parallel tuned circuit at the operating frequency.

A supply of 8-15 volts is required. The design voltage is 12 volts, at which it draws approximately 4 mA. Positive and negative supply rails are d.c. isolated from earth, allowing operation with either polarity earth. The input and output impedances are 50 ohms, although the mismatch of a 70-ohm termination is negligible. The pre-amplifier may be left on during transmission periods. This will prevent changes in junction temperature detuning the pre-amplifier at switch-on.



VK3 V.H.F. GROUP PREAMPLIFIER.



The pre-amplifier is constructed on a small (2" x 2 1/4") glass epoxy board. All capacitances below 1,000 pF. are NPO disc ceramics. Above 1,000 pF., Hi-K disc ceramics are used. Resistors up to 1/2 watt rating are suitable.

The coil formers used are Neosid Type A (single assembly) with F29 (v.h.f.) slugs. The bases usually provided have not been used, so as to maintain high unloaded tuned circuit Q. Instead, the boards are drilled 7/32" and the formers glued in. Coil details are given elsewhere.

## APPLICATIONS

Use of the pre-amplifier will result in an improvement in noise figure over even the best valve type front ends, and most transistor and FET converters. In addition, the pre-amplifier may be employed to increase overall gain to a satisfactory level.

A great improvement will result when the pre-amplifier is used ahead of the front-end of a "carphone". Most "carphones" use a 6AK5 r.f. amplifier. The best noise figure that can be expected of this tube on 2 metres is 8 dB., but a more likely figure is 11 dB. The improvement at 6 metres is less pronounced, but nevertheless worthwhile.

A word of warning is necessary in connection with "carphones". Some

"carphones" do not use an antenna change-over relay. Unless a change-over relay is installed the pre-amplifier will be damaged by excessive r.f. voltage. Installation of a change-over relay in these cases is recommended.

Similarly, the change-over relays used in a few higher power "carphones"—mainly to 25w. 3/20 type—have inadequate isolation between contacts. Damage may be prevented by connection of back-to-back diodes from input socket to earth, on the copper side of the printed circuit board. Almost any small signal diode, such as the OA95, will be adequate. This addition results in only a slight decrease in performance.

## CONSTRUCTION

The Neosid coil formers should be mounted first. File off the locating lands and glue the formers in place, making sure that the slugs will line up with the position of the cans. When the glue has hardened, the coils may be wound and the cans soldered in place, after which the remaining components may be mounted.

Ensure that all earth connections to the board are removed prior to soldering in the FET. Although no special handling precautions are necessary, for test performances the FET should be pressed down to within 1/8" of the board. For soldering, a Scope soldering iron with clean pointed instrument tip is suitable.

## COIL DETAILS

### Two Metres

C1—3.3 pF.

C2—3.3 pF.

L1—input coil, 22 S.W.G. tinned copper wire, 5½ turns tapped ½ turn from cold end (cold end being that end closest to the board).

L2—neutralising coil, 30 or 32 B. & S. enamelled copper wire, 18 turns close wound on board end of the former.

L3—output coil, 22 S.W.G. tinned copper wire, 5½ turns tapped 1½ turns from cold end.

## Six Metres

C1—10 pF.

C2—10 pF.

L1—input coil, 26 B. & S. enamelled copper wire, 10 turns tapped 2½ turns from cold end of coil.

L2—neutralising coil, 32 B. & S. enamelled copper wire, 46 turns close wound.

L3—output coil, 26 B. & S. enamelled copper wire, 11½ turns tapped 3 turns from cold end of coil.

## ALIGNMENT

With the pre-amplifier mounted in its final position, connect the supply voltage. Peak L1 and L3 for maximum gain (or in a "carphone" maximum limiter current on a weak signal), adjusting the neutralising coil (L2) where necessary to restore stability.

A number of kits will be made available by the Disposals Committee of the W.I.A. Vic. Div. Only one type of kit will be assembled, each kit containing two superfluous capacitors for the band not required. Kits will include all components—board, resistors, capacitors, FET, wire, sockets, etc. The cost will be \$6.00 including postage.

Enquiries should be addressed to:

"V.H.F. Pre-Amp."

W.I.A., Vic. Div.

P.O. Box 36,

East Melbourne, Vic., 3002.

## ACKNOWLEDGMENTS

We wish to acknowledge the original contribution to this project by the Projects Committee of the VK3 V.H.F. Group.

## REFERENCES

- (1) Orr and Johnston: "V.H.F. Handbook".
- (2) "The Real Meaning of Noise Figure," Kennedy, "Ham Radio," March 1969.
- (3) "VK3 V.H.F. Group Two Metre Converter," "Amateur Radio," February 1969.
- (4) Goodman: "Improved F.M. Operation," "Amateur Radio," April 1969.

## CARBON POTS.

A range of high quality controls designed to suit consumer, amateur and professional electronics applications having standard Australian dimensions is now available. Branded Noble, these potentiometers are individually packed in a dust-free, sealed pack. Technical data sheets on stock types are available from the Australian agents: Soanar Electronics Pty. Ltd., 30-32 Lexton Rd., Box Hill, Vic., 3128.

## PROVISIONAL SUNSPOT NUMBERS

AUGUST 1970

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa

Day	R	Day	R
1	77	15	100
2	68	17	99
3	64	18	106
4	59	19	113
5	65	20	117
6	66	21	117
7	73	22	126
8	82	23	101
9	76	24	116
10	71	25	106
11	75	26	114
12	73	27	91
13	92	28	101
14	94	29	114
15	106	30	120
		31	111

Mean equals 92.8.

Smoothed Mean for Feb 1970: 106.7.

SEPTEMBER 1970

Dependent on observations at Zurich Observatory and its stations in Locarno and Arosa

Day	R	Day	R
1	96	15	68
2	104	17	65
3	104	18	78
4	111	19	86
5	114	20	114
6	123	21	129
7	136	22	129
8	135	23	124
9	136	24	129
10	103	25	114
11	73	26	107
12	78	27	87
13	73	28	88
14	86	29	81
15	75	30	77

Mean equals 88.8.

Smoothed Mean for March 1970: 106.8.

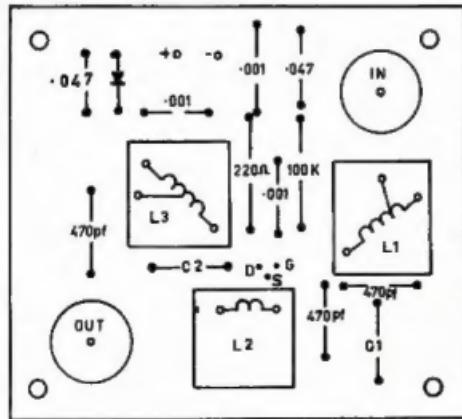
## Predictions of the Smoothed Monthly Sunspot Numbers

October 84 January 88

November 82 February 89

December 80 March 88

—Swiss Federal Observatory, Zurich.



LAYOUT OF VK3 V.H.F. GROUP PREAMPLIFIER.

## TECHNICAL ARTICLES

Readers are requested to submit articles for publication in "A.R." in particular constructional articles, photographs of stations and gear, together with articles suitable for beginners, are required.

Manuscripts should preferably be typewritten but if handwritten please double space the writing. Drawings will be done by "A.R." staff.

Please address all articles to:  
EDITOR "A.R.",  
P.O. BOX 36,  
EAST MELBOURNE,  
VICTORIA, 3002

# A SOLID STATE AMATEUR S.S.B. RECEIVER

## PART FOUR

B. G. CLIFT and A. E. TOBIN\*

This article describes the design concepts, circuit operation and construction of the second mixer and its associated crystal oscillators.

In Part One of this series, mention was made of the bands to be covered, and we must point out that an error appeared in the specification for the frequency coverage of the 10 metre band. This should read 28.0-28.5 MHz. and 28.5-29.0 MHz. Obviously a continuous coverage of 1 MHz. is more useful if it is desired to cover the v.h.f. bands with a suitable converter.

Injection frequencies for the second mixer have been chosen carefully in order to minimise the effect of spurious responses generated by the beating of higher order harmonics producing difference frequencies which may lie within the receiver pass band. In addition, it was felt that the number of crystals required should be kept to a minimum in accordance with the overall design concept.

Table 1 shows the selected crystal oscillator frequencies used for the various bands and the output frequencies from the second mixer feeding the first mixer (refer to Fig. 1 in Part One).

The v.f.o. tuning capacitor is coupled to the dial assembly so that clockwise rotation of the tuning knob (and consequently left to right movement of the dial pointer) produces backward tuning of the v.f.o. This arrangement produces forward tuning on bands 1, 2, 5 and 6.

\* Applications Laboratory, Fairchild Australia Pty. Ltd., 439 Mt. Dandenong Road, Croydon, Vic. 3136.

### CIRCUIT DESCRIPTION

The crystal oscillator and mixer 2 have been assembled on the one plug-in printed circuit board. All switching of crystals and tuned circuits associated with both sections is achieved using diodes.

The circuit configuration of the crystal oscillator is of the Colpitts type similar to that used in the v.f.o. The tank circuit is fixed tuned to 25 MHz. with a 33 pF. ceramic capacitor, the resonant frequency being reduced to 24.5 MHz. or 21.5 MHz. by switching additional shunt capacitance across the coil.

The coil is wound on a Neosid type "A" former and consists of a primary of 14 turns of 26 B. & S. enamelled wire with a 3-turn link wound over the low impedance end of the primary. The coil is fitted with a tuning slug and mounted in the normal Neosid can, but no cup or ring is used. Output from the oscillator is coupled directly into the second mixer via the 3-turn link.

The diode switching of crystals and the tank circuit is performed using standard 1 x 12 switch wafers which are assembled on a clicker plate with the ball bearings and stop removed. The switch assembly is mounted at the rear of the turret tuner and connected to the tuner shaft via a small flexible coupling. Two wafer sections are required for switching the crystals and tuned circuits of both the crystal oscillator and the second mixer. An additional wafer is required for switching the v.f.o. output between the first and second mixers.

Although only three wafers are required for the receiver, it is worth considering the addition of a further three or four wafers and the use of a clicker plate with a longer shaft if it is contemplated adding an s.s.b. exciter at a later date. This would obviate the necessity of dismantling the front end for future modifications.

It should be pointed out at this stage that the turret tuner used is an early

Band No.	Coverage	Xtal Osc.	Mixer 2 Output	Mixer 1 Output	Tuning Mode
1*	3.5 - 4.0 MHz.	—	—	9.0 MHz.	Forward
2	7.0 - 7.5 ..	21.5 MHz.	16.0 - 16.5 MHz.	9.0 ..	Forward
3*	14.0 - 14.5 ..	—	—	9.0 ..	Backward
4	21.0 - 21.5 ..	25.0 MHz.	30.0 - 30.5 MHz.	9.0 ..	Backward
5	28.0 - 28.5 ..	24.5 ..	19.0 - 19.5 ..	9.0 ..	Forward
6	28.5 - 29.0 ..	25.0 ..	19.5 - 20.0 ..	9.0 ..	Forward

Table 1.

\* For Bands 1 and 3, Mixer 2 is not used, the V.F.O. being coupled directly into Mixer 1.

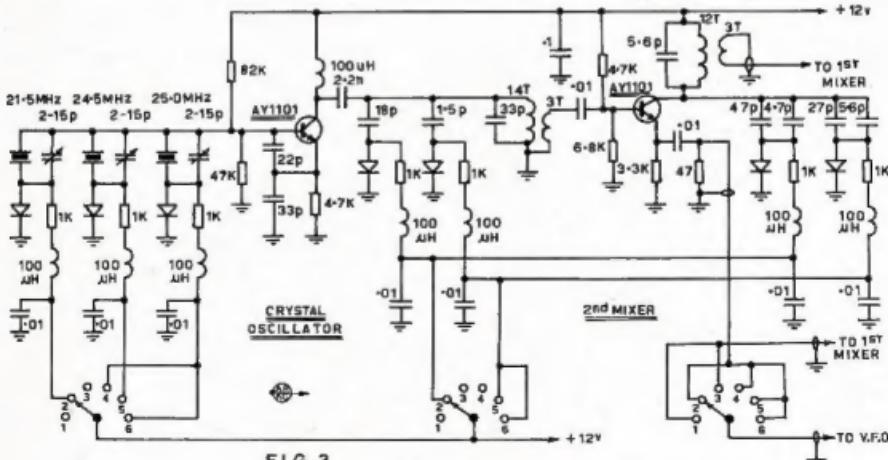


FIG. 3.

model Philips twelve channel tuner which has about  $\frac{1}{2}$ " of the main shaft protruding from the rear. Only six of the available twelve switch positions are used on account of the physical size of the coils used for the lower frequency bands.

It is, however, feasible to provide additional bands at the high frequency end if adjacent switch positions are used above 14 MHz. For example, a further 1 MHz. of the 10 metre band could be covered which would then provide a full 2 MHz. for this band. This would add to the complexity of the tuned circuit switching arrangements for the crystal oscillator and second mixer and 25.5 MHz. and 26.0 MHz. crystals would also be required. Nevertheless, this modification is quite feasible and could be added if desired.

The second mixer uses an AY1101 with a tuned collector circuit, the output being link coupled to the first mixer. The coil is wound on a Neosid type "A" former and consists of 12 turns of 26 B. & S. enamelled wire with a 3-turn link wound over the low impedance end. This coil is also fitted with a tuning slug and mounted in the normal can, but no cup or ring is used.

The tank circuit is tuned to 30.25 MHz. with a fixed 5.6 pF. ceramic capacitor. An additional 32.6 pF. is switched across the coil to retune the output to 19.5 MHz. for bands 5 and 6, and 51.7 pF. is used to retune the output to 16.25 MHz. for band 2. The final values used for these shunt capacitors may need slight adjustment, depending on individual layouts. No adjustment should, however, be made until the layout is complete and all switching diodes are installed. The diode selected for all switching functions is the AN2002. This was chosen for its very low capacitance which is typically less than 2 pF.

## CONSTRUCTION

No special techniques have been used in the construction of this section. The printed circuit board used is a universal

type board which has supply rails feeding all three sections, the top section being plain copper which may be etched with an engraving tool for r.f. circuitry if desired. However, it was found subsequently that the "dotted" sections are quite suitable for the r.f. circuitry and are easier to use. Supplies of this board may be obtained from Colt Electronics, 61 Wise Ave., Seaford, Vic.

Fig. 2 shows a photograph of the completed board. On the top section is the crystal oscillator and on the lower section is the second mixer. Not shown are the two r.f. chokes associated with the output tuned circuit of the oscillator. These are mounted on the copper side of the board. The crystals used were Hy-Q miniature type K and these were soldered directly into the circuit. Output from the v.o. (via the switch) is coupled to the second mixer using a length of 50 ohm co-ax, which was soldered directly to the circuit.

Similarly, the second mixer output to the first mixer is also via a length of 50 ohm co-ax, soldered directly to the board. To facilitate removal of individual boards, miniature printed circuit type 50 ohm co-ax sockets may be used instead. Lengths of 50 ohm co-ax should then be made up with corresponding plugs at each end to interconnect the various r.f. modules.

R.F. chokes used are Aegis single-section miniature 100  $\mu$ H., but the value of inductance is not critical.

The next article will deal with the r.f. amplifier and first mixer, which are constructed on the turret.

## COOK BI-CENTENARY AWARD

The following additional stations have qualified for the Award:

Cert.	No.	Call	Cert.	No.	Call	Cert.	No.	Call
737	IIYRK	B01	WA4VJW	848	AX3HQ			
228	WOGYM	B02	PZSHK	849	WIDDA			
759	W1BPF	B03	ZLIRHK	845	IIFPLN			
780	WSCL	B04	11WRP	848	AX3ANO			
781	JAIHBC	B05	ZM1BFR	849	WA6VOX			
782	W1DTR	B06	YV4W	850	QD7CQ			
783	DK5SD	B07	WA1JUS	851	W6QPO			
784	AX2FJ	B08	AXAKO	852	AX3HQ			
785	DK3HY	B09	GRBYI	853	WADUP			
786	W1BTU	B10	KISQM	854	YV4W			
787	W1DTR	B11	W1ZBZ	855	W1ZBZ			
788	AX1AYF	B12	ZM3JU	856	GR4US			
789	K1VZW	B13	W5RW	857	W1OB			
790	AX4XY	B14	VE3GHL	858	AX4MY			
791	K1VZWH	B15	WE2EV	859	VE3EY			
792	IIYRK	B16	W1ZBZ	860	AX3XK			
793	W1DTR	B17	W1ZBZ	861	EAKR			
794	WA4ATD	B18	W5ZGA	862	JASARA			
795	ZL2ASIM	B19	AX4UA	863	DI1CG			
796	UA0GD	B20	GSVW	864	W1FLX			
797	UW0LW	B21	YV4WOP	865	W1WYW			
798	UW0AKA	B22	W5PAJO	866	GRCDP			
799	UW0WU	B23	WAEZT	867	CH3GB			
800	AX2AMU	B24	J1AA1AT	868	VE3BLO			
801	WASCBT	B25	A5XTUX	869	AX3KA			
802	W1EHT	B26	AS2AMP	870	AX3BDQ			
803	W1DTR	B27	W1ZBZ	871	W1ZBZ			
804	W1DTR	B28	W1ZBZ	872	W1ZBZ			
805	VE5AS	B29	K7MCIG	873	W1ZBZ			
806	AX3BET	B30	ZL2RCJ	874	W1ZBZ			
807	AX3BES	B31	G3RUV	875	W1ZBZ			
808	W4CZL	B32	KP4DX	876	W1ZBZ			
809	W1DTR	B33	W1ZBZ	877	W1ZBZ			
810	W1DTR	B34	K0RTH	878	ZL4HC			
811	VE3EGT	B35	W1AIX	879	KAMG			
812	DL1IVS	B36	J1H1HWN	880	WASKPL			
813	IIYRK	B37	K1DJK	881	W1ZBZ			
814	W1DTR	B38	W1ZBZ	882	W1ZBZ			
815	ZC4MT	B39	F3EA	883	W1ZBZ			
816	AX3ALM	B40	GSWXLX	884	ZSSWH			
817	W1JAJ	B41	YT3EM	885	W3MAE			
818	VE3EAN	B42	DL1QZT	886	ZL1RKE			
819	W1DTR	B43	W1ZBZ	887	W1ZBZ			
820	OK1DKE	B44	G5BRW	888	VS3AF			
821	WA8SLD	B45	G5EDUP	889	W3YOR			
		B46	K2TUP	890				

## V.H.F./U.H.F. SECTION

The following station has qualified for the Award:

Cert. No. 4—AX3AKR

## W.I.A. V.H.F.C.C.

### New Member:

Cert. No.	Call	Confimations
76	VK1DK	109
77	VK1DK	—

### Amendment:

Cert. No.	Call	Amendment:
44	VK3AMK	157
73	VK3AMK	—

**TECHNICAL ARTICLES**

Readers are requested to submit articles for publication in "A.R.", in particular constructional articles, photographs of stations and gear, together with articles suitable for beginners, are required.

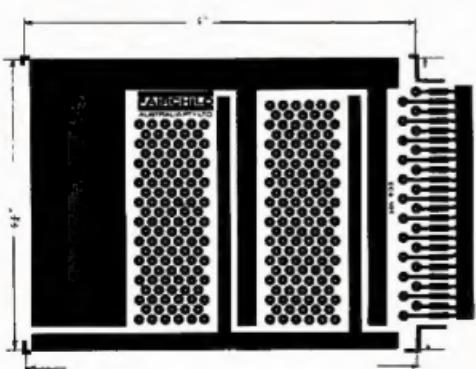


Fig. 1.

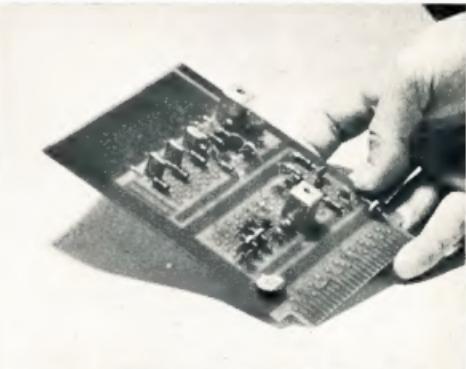


Fig. 2.—Showing printed circuit layout.

# A Signal Source for Carphone Receiver Alignment

RON HIGGINBOTHAM,\* VK3RN

The May 1969 issue of the Eastern and Mountain District Radio Club journal contained details of an extremely useful little "black box" for the alignment of f.m. carphone receivers. Since it operated from a 12v, 10 mA. d.c. supply, it held obvious attractions as a device that could be used away from power sources other than a car battery as well as in the shack for "ground based" receivers.

Another attraction was the fact that it could provide a low level signal when required (rather than having someone come up and provide carrier for your adjustments and thus occupy a net frequency).

Initial bias on the diode is obtained from the two 47K resistors across the supply rail and initial frequency adjustment is made by means of the variable capacity across the diode. Note that it may be necessary with some diodes to vary the top bias resistor until centre frequency is obtained with the trimming capacitor across the diode at half range.

On switching on the modulator the bias across the diode varies at an audio rate. This causes the capacity of the diode to change (also at an audio rate) and in turn the frequency of oscillation varies.

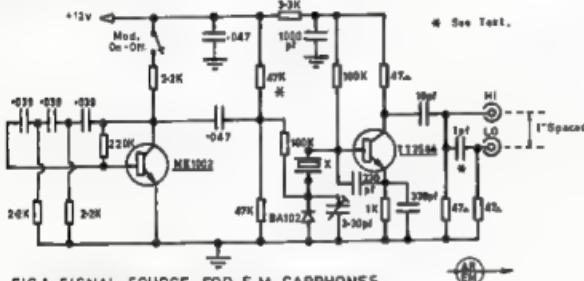


FIG.1. SIGNAL SOURCE FOR F.M. CARPHONES.

frequency unnecessarily). Moreover, since the device could use the tx crystal from the set under adjustment, there was no need to buy new crystals for it.

Basically the circuit consisted of a crystal oscillator in the 2-15 MHz. range (which produced copious harmonics useful up to and beyond the 144 MHz. band) and a simple audio oscillator modulating the oscillator by means of a BA102 diode.

The circuit was originally developed by Ken VK3AKK and gave a "high" output for initial alignment and a "low" output for final tweaking to optimum performance.

A Chinese (more or less!) copy was hooked up according to the original article, but did not modulate too well. In retrospect this failure was probably due to the very old crystal used and was no reflection on the circuit as such. However, at the time, this point was not appreciated and Les VK32BJ came to the rescue with some minor circuit changes which got the device going. The circuit used is shown in Fig. 1.

The audio side uses a MEL1002 transistor as a phase shift oscillator and with the values shown gives about a 500 Hz. note. The crystal oscillator uses a TT (or 2N) 3564 transistor and modulation is effected by the BA102 diode at the ground end of the crystal.

Two methods of construction have been used. One uses a printed circuit board and in the other system the components and transistors are mounted on tag strips which are attached to the lid of a small metal box.

In use this device has proven most useful. The only criticism is that the deviation is a little on the low side, but no doubt this could be improved by the use of a higher gain transistor in the audio oscillator, or an adjustment to the base bias. In use this slight lack of deviation has not proven any drawback.

It appears to go well with pretty well any modern crystal in the 2-15 MHz. range, but, as pointed out in the original article, older crystals such as the surplus DC11 series might need a higher gain device such as the 2N3565 in the crystal oscillator. Crystals much below 2 MHz. need different circuitry, which rather rules out the circuit as a 455 KHz. test oscillator.

Besides its utility as a signal source for the alignment of the r.f. and 1st i.f. stages of any 2 or 6 metre carphone of any make, it can also be used to line up the second i.f. stages if they are on a frequency of 2 MHz. or higher. All that is needed is a crystal of the appropriate frequency.

## CHANGE OF ADDRESS

W.I.A. members are requested to promptly notify any change of address to their Divisional Secretary—not direct to "Amateur Radio".

## DISTANCE TABLE FOR ROSS HULL V.H.F. CONTEST

	Syd.	Canb.	Bris.	Melb.	Hob.	Adel.	N.Z.	Dar.	Perth
Sydney	0	160	460	480	680	710	1300/ 1500	1950	2040
Canberra	160	0	800	290	530	670	1300/ 1500	1930	1940
Brisbane	460	800	0	880	1110	990	1500/ 1700	1790	2240
Melbourne	480	290	880	0	400	400	1500/ 1700	1930	1720
Hobart	680	530	1110	400	0	710	1300/ 1500	2280	1880
Adelaide	710	670	990	400	710	0	1900/ 2100	1620	1330
New Zealand	1300/ 1500	1300/ 1500	1500/ 1700	1500/ 1700	1300/ 1500	1900/ 2100	0	2550	3000/ 3200
Darwin	1950	1930	1780	1930	2280	1620	2550	0	1850
Perth	2040	1940	2240	1720	1880	1330	3000/ 3200	1650	0

\*43 Eleanor St. Ashburton, Vic. 3147.

# HARMONICS

## LECTURE No. 10A

C. A. CULLINAN,\* VK3AXU

- Continuing the series of lectures by C. A. Cullinan, VK3AXU, at Broadcast Station 3CS for students studying for a P.M.G. Radio Operator's Certificate.

In our discussions on alternating current in Lectures 5, 6, 7 and 8 we have spoken of sine waves although at the end of Lecture 8 we did introduce the word harmonic.

Apart from this occasion we have assumed that the sine waves have been perfect, that is, if drawn, they would assume the shape of a perfectly drawn sine curve.

However it is very seldom, if ever, that man can produce a perfect sine wave. Admittedly there are sine wave generators which produce almost perfect sine waves. For instance our A.W.A. low distortion oscillator can produce waves which are within 99.9% of perfect and there are very expensive laboratory oscillators which can do even better.

A mechanical device which produces an almost perfect sine wave is a tuning fork.

Some sine wave generators may have as little as 0.001 of 1% distortion. Measurements made of the S.E.C. mains gave a distortion figure of 4%, whilst that of a diesel alternator plant was 10%.

### HARMONICS OF MUSICAL INSTRUMENTS

Let us consider some common musical instruments such as a piano, harp and violin. Also let us assume that we have a tuning fork tuned to A440 cycles per second and that using this tuning fork as a reference we tune one of the strings of each instrument to A440. Then each of these strings is tuned to the same frequency, 440 c.p.s. However, if we strike the tuning fork, then play each instrument string we can differentiate between each instrument because each will have a distinctive sound of its own, so we can say "that's a piano" or "that's a harp" and so on.

This is because each string not only vibrates at its fundamental frequency but at a number of multiples which are known as "harmonics". It is mainly the distribution of these harmonics in relation to the fundamental frequency that gives each instrument its distinctive tone.

This may be more readily understood by comparing the energy distribution given by three musical instruments when playing Middle C = 256 c.p.s. (In concert pitch, Middle C = 273 c.p.s., French Pitch = 261 c.p.s., Scientific Pitch = 256 c.p.s.)

### Energy in Percentage

	Flute	Horn	Violin
Fundamental	13%	2%	60%
2nd Harmonic	40%	10%	8%
3rd Harmonic	10%	50%	20%
4th Harmonic	20%	15%	10%
5th Harmonic	5%	5%	2%
6th Harmonic	2%	2%	0
Remainder	10%	16%	0
Total	100%	100%	100%

From this table it can be seen, quite easily, that (for Middle C) the violin produces 60% of its total energy in its fundamental tone (also known as the 1st harmonic), and the next dominant tone is the third harmonic (256 and 768 c.p.s. respectively). However, the flute produces considerable energy at the second harmonic (512 c.p.s.) together with a considerable amount of energy at the 4th harmonic (1,024 c.p.s.), but the French horn generates half its energy at the 3rd harmonic (768 c.p.s.) whilst the fundamental is only 2%.

It is only right to point out that the instrument is an extension of the player and the sounds produced by a particular player are dependant, not only on his skill, but the quality of the instrument and its acoustic surroundings. The difference between, say, a good violinist and a poor one (using the same violin) lies completely in the subtle harmonic differences of the fundamental notes, which each player produces. Also whilst a good violinist may be able to get better sound from a poor violin he can never get the same sound as from a good instrument.

Whilst dealing with musical instruments it should be pointed out that sound is the subjective result of vibrations in the air, and that such vibrations have a special appeal to our senses when these vibrations are in the form of a sine wave or consists of a number of sine waves which have frequencies related to each other in ratios of small whole numbers such as 1:2, 1:3, 1:4, 3:4, etc.

However, a sound will be discordant if there is no such simple relationship between the frequencies, and if there are a large number of such discords the sound becomes noise.

Referring back to the table for a violin for instance, it will be noticed that this instrument produces harmonics up to the sixth and that these all bear simple ratios.

### RADIO HARMONICS

Now all this brings up a major point in audio frequency amplification and radio transmission (telephony).

We have seen that the three musical instruments mentioned in the table each produces a different sound although each is playing the same fundamental frequency, and that this difference in sound is what makes each instrument

different. This is true of all musical instruments and is also true of the human voice.

If we are to amplify or to transmit by electrical means music or speech it is essential that we do not change any of the sound of the instruments or the voice which makes the sound, because if we do so, then what we ultimately hear will not be a true reproduction of the original.

To do this it is necessary for us to pass the material through a linear system because if the system is not linear then it will generate additional harmonics which will "colour" the original material if they are strong enough in relation to the particular material, and the resulting sound may become unpleasant to the listener.

So far the discussion has been with frequencies in the audible range, but these remarks also apply to radio transmission where there may be two types of problems.

A radio transmitter generates what is known as a radio frequency wave and if the transmitter is being used for telephony then it is necessary to apply audio frequencies to the radio frequencies by one or more processes known as modulation.

The first problem is that the transmitter may generate harmonics at radio frequencies.

Usually in the interest of efficiency the transmitter will be operated in such a manner that it will generate harmonics and if these are radiated they can cause serious interference to other services.

There are some designs of transmitters where harmonics are deliberately generated, at a lower frequency than that feeding the aerial. This is usually done because it is easier to get good frequency stability at a low frequency than it is at a high one.

Well designed transmitters use considerable shielding, as well as specially designed circuits or filters, to remove harmonics as far as practicable before they reach the aerial. It must be remembered that an aerial may be designed to resonate at one particular frequency of operation, but it too will radiate harmonics at harmonic frequencies if it is supplied with them, because of insufficient harmonic suppression within the transmitter and aerial coupling circuits.

By its very nature, the oscillator in a transmitter will generate some harmonics, and the following stages of amplification will amplify these if the intermediate tuned circuits cannot remove them, thus they may get through to the final radio frequency stage for further amplification. Therefore a skillful designer will reduce these harmonics to a minimum, nevertheless the final radio frequency amplifier may generate its own crop of harmonics.

The Australian Broadcasting Control Board in its Standards for Technical Operation of Medium Frequency Broad-

casting Stations, 2nd Edition, 18th June, 1968, specifies the maximum field strength of any single frequency spurious emission (no matter what the cause).

Generally the maximum harmonic field strength permitted is 1 mV/m. at one mile from the aerial (A.B.C.B. Standards 50). Alternatively, under the I.T.U. regulations (Geneva 1959) from 1st January, 1970, the mean power of any spurious emission supplied to the transmission line must be 40 dB. below the mean power of the fundamental without exceeding the power of 50 milliwatts. Note that this applies to the input to the transmission line, not to the aerial. In some circumstances the A.B.C.B. may require far lower spurious radiation.

We have stated already that harmonics radiated from aerial systems can cause harmful interference to other services. Let us take an example. Assume that two transmitting stations are close to each other, and that the general location is close to a busy capital city port. Let these hypothetical stations operate on 912.5 KHz. and 1315 KHz.

These frequencies have been chosen to avoid embarrassment to any Australian stations as none operate on them. Also, let us assume that the first station has a measured field strength at one mile of 1 mV/m. at the second harmonic. Some calculations produce a disturbing result, so let us do these calculations.

#### Station A:

Fundamental frequency, 912.5 KHz.  
Second harmonic ( $912.5 \times 2$ ),  
1825.0 KHz.

#### Station B:

Fundamental frequency, 1325 KHz.

Now there will be two new frequencies produced by the second harmonic of A and the fundamental of B, and these can be detected by receivers tuned to each of them over a distance of possibly 15 to 20 miles. These new frequencies have been produced through the phenomenon known as Beats.

These new frequencies will be the sum and difference frequency between the second harmonic of A and the fundamental of B, and will be 3150 KHz. and 500 KHz. respectively.

This latter is the International Distress Frequency and in the circumstances outlined, considerable interference could occur to distress calls. In this case the Administration would require station A to reduce its second harmonic to a level where there would not be interference on 500 KHz.

From all this, it can be seen that radio frequency harmonics generated in a transmitter, then radiated either directly from the transmitter itself, from the transmission line, or the aerial, can cause serious interference to other services, so they are unwelcome signals.

Secondly, during the process of applying audio frequencies to a transmitter, known as modulation, it is quite possible that additional audio frequency harmonics will be generated and these will show up as distortion of the original audio frequency wave forms. If the amplitude of these is great enough the resulting transmission will be harsh

and not a faithful reproduction of the original signals.

There are two fundamental types of modulation, known as Amplitude Modulation and Angle Modulation.

Amplitude modulation is a process in which the amplitude of a transmitter's carrier wave is varied by the impressed audio frequency wave. There are several methods of achieving this.

Angle modulation is a process in which the phase angle of the carrier is varied by the impressed audio frequency wave.

Phase Modulation and Frequency Modulation are particular forms of Angle Modulation.

#### WHY ARE HARMONICS GENERATED?

Now let us ask ourselves a question, then answer it.

In an electronic audio or radio frequency system why are harmonics generated? Answer: Because the system is not linear.

Let us take a look at the reason for this. If we set up a vacuum type rectifier valve and apply increasing voltage between the anode and cathode we can measure the current flow through the valve with an ammeter connected in series in the circuit, and on squared graph paper we can plot a curve showing the relationship between impressed voltage and current flow.

It will be found that at low voltages the curve is not a straight line, then as the voltage is increased the line will become virtually straight, however at some high voltage the line will again depart from its straight form to become curved. This is where the cathode runs out of emission. (The valve may flash-over before this point is reached.) This is the elongated S of Fig. 1a. The general shape of the curve is the same for all high vacuum rectifiers although the slope may differ between different valve types. All of these remarks apply to a half-wave rectifier, and after all a full wave vacuum tube rectifier consists of two half-wave rectifiers in the same envelope.

An examination of this curve reveals that there is a linear relationship between applied voltage and the current passed over most of the curve, but at both ends there is a marked departure from the linear condition.

This curve is, also, a generalised curve for a valve amplifier valve hav-

ing sufficient bias to cut-off the plate current, and which runs out of cathode emission at the other end of its curve.

As an example, we may take the case of a class C stage of a plate modulated telephony transmitter. The class C amplifier operates with a very high grid bias, several times that needed for plate current cut-off. The a.c. modulating voltage adds or subtracts to the d.c. plate voltage so that at 100% positive modulation the peak plate voltage is double the d.c. plate voltage, whereas on the negative swing of the modulating voltage this subtracts from the d.c. plate voltage with the result that at this point it exactly cancels the d.c. plate voltage.

If the class C amplifier stage has been properly set-up, and an analysis is made of the resultant modulated wave at 100% modulation with, say, an audio frequency of 1,000 Hz. then it will be observed that the wave is symmetrical, that is both positive and negative sides (peaks) are the same. This measurement can be done best when a sine wave is used for modulation, with a cathode-ray oscilloscope, or with an amplitude modulation monitor.

However, after some considerable time, it may be found that the positive and negative peaks are no longer the same, that is the wave is not symmetrical, also that there is serious harmonic distortion.

Although the d.c. plate current is still the same, assuming that there has not been any change in the adjustment of the transmitter, then it will be found that whilst the negative half of the modulating voltage can take the class C amplifier to 100% negative modulation, the positive modulating voltage cannot raise the amplifier to 100% positive modulation.

What has happened is that the class C amplifier valve has started to lose cathode emission and the loss can only be detected when the plate voltage is swung high in a positive direction by the modulating voltage. The class C stage valve is then operating in the top curved position of the curve in Fig. 1a.

It is only proper to state that this is the loss of peak cathode emission. If the valve or valves causing the asymmetrical modulation are left in use the emission will drop to the stage where it becomes apparent due to lower than normal d.c. plate current.

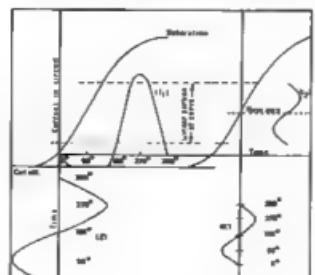
It may not be clear from the diagram in Fig. 1a that the elongated S current curve is derived by applying various d.c. voltages to the valve.

If an a.c. voltage is applied then no part of the curve can be completely straight simply because there are no two successive points in a sine wave which make a straight line. Theoretically this can be taken to two consecutive electrons and is due to the fact that the angle of the current is continuously changing, whether we consider this change in single degrees, or say one millionth of a degree.

The sine curve of Fig. 1a when projected via the elongated S current curve produces the current curve II of Fig. 1a.

The student should draw these curves to satisfy himself.

In Fig. 1a we have shown, too, a sine wave whose axis passes through



the current curve slightly to the right of the cut-off point. By extending the sine wave curve upwards, to where it intersects the current wave we can plot a graph or curve of the current which flows in the valve due to the excitation by the sine wave. As this wave proceeds from  $0^\circ$  to  $45^\circ$  in a negative direction, the valve is driven to the cut-off point then past this position so no current can flow in the circuit.

It will be noticed that a small amount of current will flow between  $0^\circ$  and approximately  $45^\circ$  since the cut-off point corresponds to approximately  $45^\circ$ .

From  $45^\circ$  to  $90^\circ$  the valve is driven past cut-off so no current can flow.

After  $90^\circ$  the exciting voltage starts to drop to zero at  $180^\circ$ . However when it reaches  $135^\circ$  it has come back to the cut-off point, so that from  $135^\circ$  to  $180^\circ$  a small amount of current may flow. It must be remembered that although the exciting wave is now in a conducting portion of the valve curve, the exciting voltage is, itself, falling to zero until at  $180^\circ$  there is no exciting voltage, hence no current.

As the exciting voltage ( $E$ ) increases in a positive direction from  $180^\circ$  to  $270^\circ$ , the valve will conduct so that current flows in the valve.

This is shown in curve (II) Fig. 1a.

But it will be seen that as the exciting wave approaches  $270^\circ$  the current (II) does not increase in proportion and (II) does not regain its shape until after the exciting voltage has passed  $270^\circ$ .

Curve (II) between the lines marked "linear portion of curve" appears to be a straight line on each side and can be considered linear, but the parts outside the linear portions are curved and it is operation in these regions that produce harmonics.

It will be noted, too, that the curve (II) is far from the same shape as the exciting voltage curve ( $E$ ), in fact it is approximately only half of it.

This is the type of curve we get when a rectifier valve changes a.c. into d.c., when an amplifier, whether audio or radio frequency distorts or when a frequency multiplier is used in a transmitter to produce high frequency from a lower one by harmonic multiplication.

Now let us look at Fig. 1b. The elongated S curve is the same as that of Fig. 1a (as near as we could draw it and means exactly the same). But this curve is taken to represent an amplifier valve, not a rectifier.

An amount of negative bias has been applied to the grid of the valve so that its operating point is half way along the linear portion of the curve.

Now if an a.c. exciting voltage ( $E$ ) is applied and its maximum negative and positive peaks do not pass beyond the limits of the linear portion of the curve, then the resultant curve (II) will have an identical shape to the shape of the exciting voltage ( $E$ ). Its amplitude may be greater or lesser depending on whether the valve has a gain greater than unity, but the shape will be similar, i.e. if ( $E$ ) is a sine-wave, then (II) will be a sine-wave.

Now, if the exciting voltage  $E$  is increased in amplitude its negative and

The frequencies of all the stations mentioned in this lecture were as stated at the time the lecture was written. However, with the passage of time, some station frequencies may change, therefore any Amateur wishing to calibrate equipment by using b.c. stations as frequency references should verify the frequency of each station beforehand. A list of stations may be obtained from the Australian Broadcasting Control Board, 373 Elizabeth Street, Melbourne, Vic. 300.

positive peaks will exceed the linear portion of the current curve and (II) will no longer be a sine-wave as its negative and positive peaks will be flattened as shown in the half cycle (II) of Fig. 1a. Distortion will result as harmonics will be produced.

Also, if instead of altering the amplitude of the exciting voltage ( $E$ ), the bias points (new axis) is moved, then again the resultant wave will not be symmetrical.

Notice should be taken in Fig. 1a and 1b that although the current curve is the same in both, amplitude of the exciting voltage ( $E$ ) has been reduced to make it fit the linear portion of the current curve.

The student should draw these curves, also draw a larger sine-wave ( $E$ ) and plot this when he will find that the peaks of the plotted current curve are flattened as has been stated.

To show how harmonics distort a pure sine-wave, Figs. 2 and 3 should be examined. In Fig. 2 the single cycle represents a sine-wave. Superimposed on this is a smaller amplitude wave of two cycles, this being the second harmonic of the sine-wave. Actually this is a co-sine-wave, that is one which reaches its maximum value  $90^\circ$  electrical degrees before a sine-wave would do so. However, it is important to realise that in Fig. 2 there are two cycles of the co-sine-wave and only one cycle of the sine-wave. A single

cycle co-sine-wave would be shown starting with maximum current of  $0^\circ$ .

In order to illustrate the effect of a second harmonic on its fundamental (1st harmonic) the maximum amplitude of the second harmonic has been made about 37% of the fundamental, this being the most that could be drawn in the space available.

A second harmonic of this magnitude will greatly modify the fundamental and normally such a harmonic would not be found in any form of electrical reproduction unless the equipment is badly out of order. This statement does not apply to transmitters where frequency multiplication is used. Also, it does not apply to musical instruments (as already shown) including those using electrically generated tones.

The manner in which the second harmonic modifies the fundamental may be found by adding, algebraically, the amplitudes of the fundamental and the second harmonic at any given time (electrical degree), remembering that those parts of the curves above the axis are positive and those below are negative.

It will be observed that at  $90^\circ$  the maximum positive portion of the first cycle of the second harmonic will subtract from the maximum of the fundamental so that the amplitude of the latter is greatly reduced. However, the maximum positive portion of the second cycle of the harmonic adds to the maximum positive portion of the fundamental, thus increasing it.

This means that the original sine-wave of Fig. 2 is no longer symmetrical, hence it is distorted.

The curves of Fig. 2 have been added together and produce the curve shown in Fig. 3. Note that the negative portion of the sine-wave of Fig. 2 has been greatly reduced in amplitude and that it has been grossly flattened. On the other hand, the amplitude of the positive half has been increased considerably, although its base line is the same, and its shape has changed a little too.

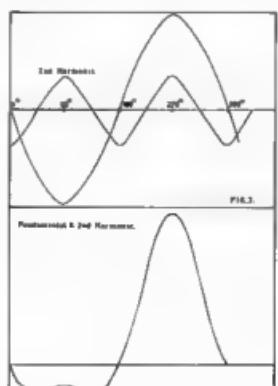
So this is what happens to a wave having a large second harmonic.

Actually its general shape in the positive direction closely resembles that of the current wave II of Fig. 1 (the drawing scales are not the same) and this proves what we set out to prove, namely, that a rectifier can produce considerable harmonic distortion, as can a valve rectifier which is either wrongly biased or has too great an exciting voltage on its grid.

For simplicity, Figs. 2 and 3 do not show other harmonics, but the student can add these. For instance, three cycles of 3rd harmonic can be drawn in Fig. 2. The first cycle can start in a positive direction at  $0^\circ$  with maximum at  $30^\circ$ , maximum negative will be at  $90^\circ$  and so on. Again for simplicity this could be made, say  $10^\circ$  of the fundamental. Then Fig. 3 can be replotted using the figures or dimensions obtained by adding together the fundamental, 2nd and 3rd harmonics when it will be seen that there are more changes in the overall shape of Fig. 3.

It is rather difficult to draw, graphically, and specially at low levels, any further harmonics.

(to be continued)



# John Moyle Memorial National Field Day Contest, 1971

SATURDAY, 13th FEBRUARY, TO SUNDAY, 14th FEBRUARY, 1971

The Federal Contest Committee of the Wireless Institute of Australia invites all Australian Amateurs and Short Wave Listeners to participate in this Annual Contest, which is held to perpetuate the memory of John Moyle, whose efforts advanced the Amateur Radio Service.

There are two divisions of this Contest, one of 24 hours continuous duration, and one of 6 hours continuous duration. The six-hour period has been included to encourage the operator who is unable to participate for the full 24-hour period. The 24-hour continuous operation is to be chosen by operator from 24-hour period.

Operators using 25 watts or less input to the final stage will be considered for a certificate where his activity warrants its issue.

## DATES

From 0600 GMT, 13th February, 1971, to 0800 GMT, 14th February, 1971.

## OBJECTS

The operators of Portable and Mobile Stations within all VK Call Areas will endeavour to contact other Portable/Mobile and Fixed Stations in VK Call Areas and Foreign Call Areas.

## RULES

1. There are two divisions, one of six (6) hours, and one of twenty-four (24) hours duration. The six-hour period for operating may be chosen from any time during the Contest, but the six-hour period so chosen must be continuous. In each division, there are also sections:-

- (a) Portable/Mobile Transmitting, Phone.
- (b) Portable/Mobile Transmitting, C.W.
- (c) Portable/Mobile Transmitting, Open.
- (d) Portable/Mobile Transmitting, Multiple Operation, open only.
- (e) Fixed Transmitting Stations working Portable/Mobile Stations, open only.
- (f) Reception of Portable/Mobile Stations.

2. All Australian Amateurs are encouraged to take part. Operators will be limited to their licensed power. For Portable entries, power shall be derived from a self-contained and fully portable source.

(a) Portable/Mobile Stations shall not be situated in any occupied dwelling or building. Portable/Mobile Stations may be moved from place to place during the Contest.

No apparatus shall be set up on the site earlier than 24 hours prior to the Contest.

All Amateur bands may be used, but no cross band operating is permitted. Cross mode operation is permitted.

Entrants in Section (d) for Multiple Operator Stations can set up separate transmitters to work on different bands

at the same time. All such units of a Multiple Operator Station must be located within an area that can be encompassed by a circle not greater than half a mile diameter.

For each transmitter of a Multiple Operator Station a separate log shall be kept with serial numbers starting from 001, and increasing by one for each successive contact. All logs of a Multiple Operator Station shall be submitted by the operator under whose Call Sign the transmitters are working. No two transmitters of a Multiple Operator Station are permitted to operate on the same band at any time.

3. Amateurs may enter for any section.

4. One contact per station for phone to phone, also one for c.w. to c.w. per band is permitted. Cross mode operation will be accepted for scoring.

5. Entrants must operate within the terms of their licences and in particular observe the regulations with regards to portable operation.

6. For VK stations contacting VK stations, the exchange of serial numbers consisting of RS or RST report plus three figures commencing with 001 and increasing by one for each successive contact by the VK station shall be proof of contact. The exchange of RS or RST reports only with non-VK stations shall be sufficient proof of contact for this contest.

### Scoring—

#### (a) Portable/Mobile Stations:

For contacts with Portable/Mobile Stations outside entrant's Call Area ..... 13 points

For contacts with Portable/Mobile Stations within entrant's Call Area ..... 10 points

For contacts with Fixed Stations outside the entrant's Call Area ..... 5 points

For contacts with Fixed Stations within the entrant's Call Area ..... 2 points

#### (b) Fixed Stations:

For contacts with Portable/Mobile Stations outside entrant's Call Area ..... 13 points

For contacts with Portable/Mobile Stations within entrant's Call Area ..... 10 points

Operation via active repeaters or translators is not allowed for scoring purposes.

### Example of Victorian S.W.'s Log

Date (DD/MM)	Time (GMT) (hrs)	Band	Call Sign Used	No. Sent	RST Worked	Pts Clim
13/2/71	0600	20	VK2AAH/P	58001	VIC3ATL/P	15
	0610	20	VIC3ATL/P	58006	VIC3QV	10
	0620	40	VK2AAH/P	580004	VIC3NFP/P	15
	0640	20	VIC3QV	58010	VIC3QX/P	5
	0650	20	VK4OFP/P	58040	VIC3QX/P	15

\* No claim Fixed Station.

8. The following shall constitute Call Areas: VK1, VK2, VK3, VK4, VK5, VK6, VK7, VK8, VK9 and VK10.

9. All logs shall be set out under the following headings: Date/Time (G.M.T.), Band, Emission, Call Sign, RST/No. Sent, RST/No. Received, Points Claimed. Contacts must be listed in numerical order.

In addition, there shall be a front sheet showing the following information:-

Name ..... Address  
Call Sign ..... Section .....  
Division ..... (6-hour or 24-hour)  
Points Claimed .....  
Call Sign of other op/s (if any) .....  
Location of Portable/Mobile Station .....  
From ..... hours to ..... hours

A brief description of equipment used, and points claimed, followed by the declaration:

"I hereby certify that I have operated in accordance with the rules and spirit of the Contest."

Signed ..... Date .....

10. The right is reserved to disqualify any entrant who, during the Contest, has not observed the Regulations and the Rules of this Contest, or who has consistently departed from the accepted code of operating ethics.

11. The decision of the Federal Contest Manager of the Wireless Institute of Australia is final and no dispute will be entered into.

12. Certificates will be awarded to the highest scorer of each section of each division. Additional certificates may be issued at the discretion of the F.C.C. The six-hour certificates cannot be won by a 24-hour entrant.

### 13. Return of Logs:

All entries must be postmarked not later than 7th March, 1971, and be clearly marked "John Moyle Memorial National Field Day Contest, 1971" and addressed to:

Federal Contest Manager, W.I.A.,  
Box N1002, G.P.O.,  
Perth, W.A. 6001.

### RECEIVING SECTION

14. This section is open to all Short Wave Listeners in VK Call Areas. The Rules shall be the same as for the Transmitting Stations, but may omit the serial number received.

Logs must show the Call Sign of the Portable/Mobile Station heard, the serial number sent by it, and the Call Sign of the Station being worked.

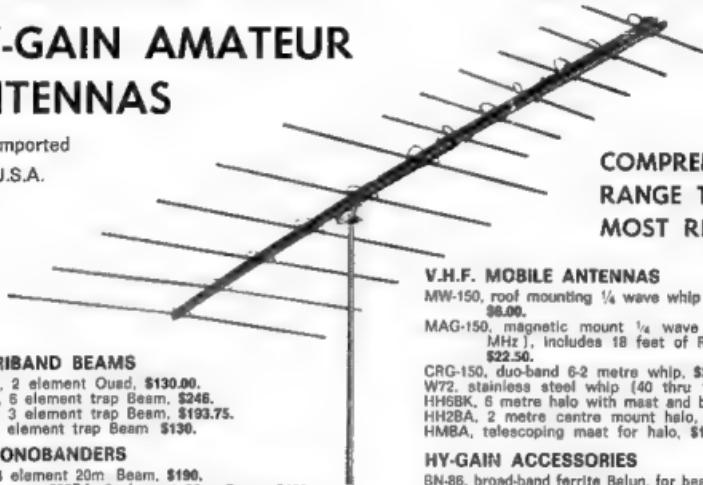
Scoring will be on the same basis as for Transmitting Stations. It will not be sufficient to log a station calling CQ. A portable/mobile station may be logged once only for phone and once only for c.w. in each band.

Awards: Certificates will be awarded for the Highest Scorer in each Call Area, for the 6-hour and the 24-hour divisions.

# Season's Greetings to all Readers

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TH3MK3, 3 element trap Beam, \$193.75.  
TH3Jr, 3 element trap Beam \$130.

### H.F. MONOBANDERS

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203BA, 3 element 20m. Beam, \$150.  
153BA, 3 element 15m Beam, \$94.

### H.F. VERTICALS

14AVO, 10m thru 40m trap Vertical, \$59.  
18AVO, 10m. thru 80m. trap Vertical, \$85.  
18V, 10m. thru 80m base loaded Vertical, \$36.50.

### H.F. MOBILE WHIPS AND FITTINGS

HMM, mobile mast assembly, \$19.50.  
MC Series coil and adjustable tip-rod assemblies.  
MC-75, 80m., \$25.00 MC-20, 20m., \$18.75  
MC-40, 40m., \$19.50 MC-10, 10m., \$14.50  
MC-15, 15m. \$16.60

BPR, bumper mount, \$12.50.

BDYF, body mount, \$9.00.

SPG, heavy duty spring, \$12.50.

SPGM, light duty miniature spring, \$6.00.

OD, quick disconnect accessory for mobile whips, \$6.00.

JMS, "Jiffy" body mount, \$9.00.

Also Body mount co-ax adaptors, gutter clips, whip fold-over adaptors.

### V.H.F. ANTENNAS

23, 3 element 2m. Beam, \$15.  
28, 8 element 2m. Beam, \$29.50.  
215, 15 element 2m Beam, \$59.  
SGP, 2m ground-plane, \$12.50.  
GPG-2, 2m  $\frac{1}{2}$  wave ground-plane, \$23.  
GP-50, 25 thru 54 MHz. ground-plane, \$23.

### V.H.F. MOBILE ANTENNAS

MW-150, roof mounting  $\frac{1}{4}$  wave whip (108 thru 470 MHz.), \$6.00.

MAG-150, magnetic mount  $\frac{1}{4}$  wave whip (108 thru 450 MHz.), includes 18 feet of RG58U and connector, \$22.50.

CRG-150, duo-band 6-2 metre whip, \$38.00.  
W72, stainless steel whip (40 thru 100 MHz.), \$15.75.  
HH6BK, 6 metre halo with mast and bumper mount, \$34.50.  
HH2BA, 2 metre centre mount halo, \$12.50.  
HMBA, telescoping mast for halo, \$12.50.

### HY-GAIN ACCESSORIES

BN-86, broad-band ferrite Balun, for beams and doublets, \$22.  
LA-1, Lighting Arrestor, for installation in standard 52 or 72 co-axial feedline, designed to Mil. specs., \$37.  
EI, End Insulators, for doublets, \$2 per pair.  
CI, Centre Insulator, for doublets, \$7.50.

### OTHER ACCESSORIES

Digital Electric Clocks.

"Solaris" (Italian), 24-hour, large figures, \$29.00.  
"Caslon" (Japanese), 12- and 24-hour, \$24.50.

EK-26, Katsumi Electronic Keyer, \$75.00.

K-109, Kyoritsu dual impedance 52 and 75 ohm SWR meter, \$21.00.

PS-750, PIC single-pole, 5-position co-axial line RF switch, \$21.50.

PS-751, PIC two-pole, 2-position co-axial line RF switch, \$16.50.

PS-752, PIC single-pole, 2-position co-axial line RF switch, \$15.50.

1100M Emotator heavy duty antenna rotator, base mount, \$148.50; pipe mount, \$165.00.

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80-10 mx, peak In. 300w.

**FTDX-400 TRANSCEIVER:** 80/10 mx, PA two x 6KD6, 560w. peak input SSB, choice of manual, PTT or VOX operation. Full coverage on 10 mx, offset tuning, calibrator. Includes PTT mic. \$595.

**FTDX-500 TRANSCEIVER:** Now available here, this model (as sold in U.S.A.) is similar to the FTDX-400, with a different panel layout. PA two x 6KD6, 560w. peak input SSB. CW and SSB modes. Includes PTT mic. \$595.

**FV-400 EXTERNAL VFO:** For FTDX-400 and FTDX-500. \$88.

**FT-101 TRANSCEIVER:** Successor to the famous FTDX-100, 80/10 mx, SSB, AM, CW PA two x 5J56A, 300w. peak input SSB. Built-in dual AC/DC power supply. Low current drain, transistorised except for transmitter driver and PA. Plug-in modules, IF noise blanker, FET receiver RF, clarifier, built-in speaker. Ideal for portable/mobile from 12v. DC, or in the shack on AC. \$875.

**FT-101 EXTERNAL VFO:** Matching auxiliary VFO for the FT-101. \$86.

**FT-200 TRANSCEIVER:** 80/10 mx, PA two x 6JS6A, 300w. peak input SSB. Manual, PTT or VOX control, offset tuning, calibrator. Operates from a separate power supply. \$330.

**FP-200:** Yaesu AC Power Supply for FT-200, in matching cabinet with in-built speaker. \$30.

**DC-200:** Yaesu 12v. DC Power Supply for FT-200, complete with special pug and cable. \$120.

- ★ C.W.—Yaesu equipment is ideal for C.W. operation. Listen on the C.W. bands and judge for yourself.
- ★ Receiver resolution of S.S.B. signals is surprisingly easy.
- ★ With the exception of FT-200 and FTV-850, all sets feature built-in power supplies.
- ★ All sets are checked and tested before despatch, and three-core A.C. power cords are fitted.

All Prices Include Sales Tax. Freight is extra.

Prices and specs. subject to change without notice

## BAIL ELECTRONIC SERVICES

60 SHANNON STREET, BOX HILL NORTH,  
VIC., 3129. Telephone 89-2213

N.S.W. Rep.: STEPHEN KUHL, P.O. Box 56, Mascot, N.S.W., 2020. Telephone: Day 67-1650 (AH 37-5445)  
South Aust. Rep.: FARMERS RADIO PTY. LTD., 257 Angas St., Adelaide, S.A., 5000. Telephone 23-1268  
Western Aust. Rep.: H. R. PRIDE, 26 Lockhart Street, Como, W.A., 6152. Telephone 60-4379

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## RACAL WINS FAIRCHILD PLANAR AWARD WITH NEW POWER AMPLIFIER

The 1970 Fairchild Planar Award, presented annually for practical application of semiconductors in a unique concept or design, has been won by Racal (Aust.) Pty. Ltd., who entered a power amplifier which is used in their range of high quality, high frequency s.s.b. transceivers.

The award, a bronze plaque featuring an engraved micro-circuit design, was presented to Mr. John Jackson, Chief Engineer of Racal, by Mr. John Baldwin, General Manager of Fairchild (Aust.) Pty. Ltd., at a function at the Wentworth Hotel, Sydney, on November 11, 1970.

"We believe that this amplifier was the first commercially available fully solid state 100 watt linear high frequency amplifier in the world," said Mr. Jackson, accepting the award.

Transceivers incorporating the new technology are now exported worldwide. They are also used extensively in Australia, particularly for post office out-back radio stations.

Presenting the award, Mr. Baldwin said, "The enterprise shown by Racal engineers in designing and developing this range of transceivers, and in winning the Planar Award, is just further evidence of the potential we have in Australia. When we tackle challenges in the right way, we take our place among the world's leading technological nations."

## A & R-SOANAR GROUP APPOINTMENT

Mr. Barry T. Houston has joined the A & R-Soanar Electronics Group, Box Hill, Vic., as a transformer design and development engineer, where he will be engaged on forward research and development activities.

Formerly Mr. Houston was a design engineer with L. M. Ericsson Pty. Ltd., Trimax Division, and Thorn Electrical Industries Pty. Ltd.

# INCREASE IN AMATEUR LICENCE FEES

Following the increase of Amateur licence fees from \$2 per annum to \$6 per annum announced in the last Budget, the following telegram was sent by the Institute to the Postmaster-General:

"The Wireless Institute of Australia refers to the Wireless Telegraphy Regulations Bill and asks that licence fees increase to \$8 be reviewed. Our request is justified on the following grounds—"

1. The Amateur Service deserves special consideration because of community interests served in disasters.
2. The Amateur Service educates and encourages technical expertise.
3. Amateurs have no recourse to claim licence fees as a tax deduction.
4. The Wireless Institute is the only organisation representing a licensed communication service. By co-ordinating individual requests and with strict self-policing controls, the Department's costs associated with the administration and technical supervision are minimal.

We urge favourable reconsideration of the proposed licence fee increase."

"As addendum to previous telegram, many Amateur licensees are pensioners and should be accorded similar concessions to those who presently enjoy as holders of broadcast and television viewers' licences."

—Peter D Williams, VK3HZ,  
Federal Secretary.

The following is the Postmaster-General's reply to the Institute:

Postmaster-General,  
Canberra, A.C.T. 2600

Dear Mr. Williams,

I refer to your lettergram of 8th October, 1970, concerning the proposed increase in licence fees for amateur radio stations.

The existing licence fee for all types of radio-communication stations has remained unchanged at \$2 per annum since 1954. In the years before 1954 when stations were few, the revenue from amateur stations provided a medium for emergency communication, ships, aircraft and police revenue did not match costs, but the difference was not great enough to cause concern. Since 1954, however, developments in technology have enabled amateurs to have a wide-scale expansion in the use of radio communication in the commercial and other fields. There are now more than 135,000 licensed stations of every type operating under diversified rules designed to minimize the risk of interference and conduct of services generally. At the same time the disparity between licence fee revenue and costs has continued to increase to a point where it was essential to introduce measures to restrain the increase. It must be kept in mind that money values have changed so that the fee of \$2 which has applied since 1954 is the equivalent of \$7 today.

There have been developments in amateur radio corresponding to those referred to above. In 1964, for instance, there were only 335 licensed amateur transmitting stations using quite limited operating techniques. Today there are now over 3,000 comprising stations using a far greater range of techniques than in earlier years. Today, amateur licensees are authorized to pursue experiments in the UHF, O.H.F. and S.H.F. bands, to undertake television experiments, and to employ single sideband and pulse transmissions. Amateur licensees, as you know, also now engage in experiments involving moon reflected signals and communication satellites.

In determining the new fee structure, which will apply to all radio services account was taken of the fact that the costs associated with the licensing and surveillance of land and fixed stations are greater than those associated with stations in the mobile category and, as you probably are aware, the fee for the former will be \$10 and for the latter \$6 per annum.

Although the large majority of amateur stations are immediately below the \$6 fixed category it was decided that their confinement to experimental and non-commercial activities warranted special consideration and that they should be included in the \$6 category.

Although it is appreciated that the amateur service is self-regulated to a large degree, my

Department is required, in return for this fee, to grant licences, issue and record call signs, inspect stations, investigate complaints, arrange for reciprocal agreements with other countries, frequency measure and monitor transmissions as required and liaise with other Administrations and the International Telecommunications Union in regard to amateur radio matters generally.

I can assure you that I am well aware of the part which amateur radio operators have played and are continuing to play in providing emergency communications during national emergencies. I also appreciate the encouragement given to the study of the radio art through amateur radio activities. At the same time I regret to advise that the Government cannot continue to subsidize the administration of amateur radio stations to the extent that it has done for the recent years and that the way is not clear, therefore, to reduce the new fee of \$6.

The increased fees for licences will still not meet the discrepancy between revenue and costs and for this reason I am afraid it would be impractical to introduce concession fees for pensioner amateur station licensees as requested. As you will appreciate, the grants of such a concession would make it most difficult to reject claims by other amateur operators who may consider their situation warrants a similar concession.

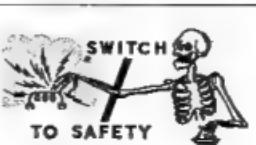
Yours sincerely,

Alan S. Hulme,  
Postmaster-General.

## NEW CALL SIGNS

JULY 1970

VK1BS—B. A. Stevens, 28 Adair St, Scullin, 2614.  
 VK2AII—E. Law, 20 Bonarre Rd, Gymea, 2227.  
 VK2AOW—R. J. Wirth, 22 Berry St, Cronulla, 2290.  
 VK2AQH—J. Clarke, 478 Lane Lane, Broken Hill, 2880.  
 VK3BIC—D. M. Watkins, 63 Bestrice St, Balgowlah Heights, 2093.  
 VK2BMB—R. A. Balch, 34 Dress Circle Rd, Avalon, 2107.  
 VK2BRB—J. Wippel, 25 Judge St, Sandwick, 2031.  
 VK22IL—K. J. Hargraves, 18 Marks Pt Rd, Marks Point, 2280.  
 VK2KK—G. L. May, 34 Walsh Ave, Maroubra, 2025.  
 VK2ZPV—P. S. Vogel, 5 Wilson St, Maroubra, 2025.  
 VK2ZQH—P. J. Chappell, 4 Gallop Ave, Parkes, 2870.  
 VK2ZW—P. Coates, 66 Ferrier St, Lockhart, 2556.  
 VK3GM—T. G. Foster, 603 Sebastopol St, Ballarat, 3350.  
 VK3JE—J. Bay, Station: 3 Allison Rd, Mount Eliza, 3930; Postal P.O. Box 34, Clayton, 3160.  
 VK3JU—L. Cunningham, 4 Kustace St, Wenvoe, 3355.  
 VK3AEZ—J. McI. Vale, 905 R. Alexander Rd, Essendon, 3040.  
 VK3AJQ—J. E. Field, 27 Reignate Rd, Highgate, 3115.  
 VK3BAO—R. J. Malcolm, Boldstoke, 3880.  
 VK3BDQ—J. K. Horan, 34 Roberts St, Glen Waverley, 3150.  
 VK3DU—H. E. Westerhof, Army Appren-tice School, Balcombe, 3833.  
 VK4FV—P. W. Fowler, 19 Orstes Rd, Yeronga, 4104.  
 VK4HQ—L. P. Crowe, 4 Orvicio Tce, Caloundra, 4551.  
 VE4KI—R. E. Rutherford, 7 White St, Nerrang, 4211.



VK4VA—V. F. Burman, 4 Mays Cr., Aitken-ville, 4211.  
 VK4CF—F. Russell, Station Raintree Ave, Victoria Estate, 4266, Postal C/o P.O., Victoria Estate, 4850.

VK4GA—G. T. Adamson, 3 Maker St, Toorak, 3130.  
 VK4YL—W. V. Bulman, 4/82 Apollo Rd, Bulimba, 4175.  
 VK4VV—M. R. Rhyse-Williams, Station: Little Ship Club, Dunwich, 4165, Postal C/o Post Office, Dunwich, 4163.

VK4ZA—R. E. Isaac, 112 Auckland St, Gladesville, 4090.  
 VK4ZLR—R. Longmead, 38 Morrow Rd, Taringa, 4035.  
 VK4ZMJ—M. J. Joyce, 38 Trout St, Camp Hill, 4152.

VK5EN—R. A. R. Nitashke, 3 Hall St, Cummins, 5051.

VK5JP—E. J. Willis, 5/884 Glynhurst Rd, Kensington Gardens, 5068.

VK5ST—N. S. Schahinger, 77 The Grove, Upper Mitcham, 5052.

VK5ZD—R. E. Miller, 15 Brigalow Ave, Blackwood, 5051.

VK5ZFC—D. A. Gaesser, 59 Russell Tce, Woodville Park, 5011.

VK5ZG—P. W. Douglas, 138 Flinders Tce, Port Augusta, 5700.

VK5ZPA—P. A. Reichel, 38 Gray St, Killenny, 5000.

VK5ZBQ—R. E. Davies, Falls Rd, Leamurde, 5078.

VK5MLT—Technical College Radio Club, Harold St, Mt Lawley, 6054.

VK5VE—The South Australian Amateurs Group, Blue Waters, Little Grove, Albany, 5230.

VK5CIE—F. W. Fletcher, Station: Portable; Postal: 53 Ivan Park, Ringwood, Englefield, 3135.

VK5ZA—D. Dragg, 1/409 Cambridge St, Floreat Park, 6014.

VK1ZGD—G. de Groot, C/o Hytton Hall, University of Tasmania, Sandy Bay, 7000.

VK5CW—C. F. Williams, 34 Memorial Dr., Alice Springs, 3750.

VK5ZFH—G. L. Stephens, 8/1371 Sergions Cr., Rapid Creek, 2798.

## CANCELLATIONS

VK1EA—R. M. Miles, Not renewed.

VK1DD—R. D. Davies, Not renewed.

VK1VB—V. F. Burman, Now VK4VA.

VK1ZAV—R. D. Asell, Not renewed.

VK1ZJM—J. Hyne, Transferred to Vic.

VK1ZRN—R. W. Nash, Now VK3ZRL.

VK2BA—B. A. Chapman, Deceased.

VK1OK—J. W. Smith, Deceased.

VK1OK—A. M. Manwarrie, Deceased.

VK2ZS—W. J. Smith, Transferred to W.A.

VK2ZL—S. U. Grimmett, Not renewed.

VK2AQL—J. Lee, Deceased.

VK2AR—R. W. Ross, Deceased.

VK2ARQ—A. Raynor, Deceased.

VK2BAD—D. A. Davis, Transferred to A.C.T.

VK2BAW—G. F. Vierstrehuizen, Not renewed.

VK2BES—A. S. Stevens, Now VK5ES.

VK2BEB—B. C. Chisholm, Not renewed.

VK2BZR—B. H. Ridley, Not renewed.

VK2ZDE—A. Day, Not renewed.

VK2ZDR—D. G. Hosking, Not renewed.

VK2ZG—J. Clarke, Now VK1QAD.

VK2ZG—R. J. Clarke, Now VK1QAD.

VK2ZQA—R. J. Irving, Not renewed.

VK2ZQJ—P. R. Lorenzen, Not renewed.

VK3ELW—L. McD. Stone, Transferred to N.S.W.

VK3VE—V. W. Harrison, Not renewed.

VK3YQG—E. Smith, Transferred to A.C.T.

VK3YQH—E. Smith, Transferred to A.C.T.

VK3ASC—J. W. Brown, Not renewed.

VK3AVZ—C. A. Trotter, Transferred to N.S.W.

VK3AZH—K. J. Horstal, Not renewed.

VK3JAR—R. J. Malcolm, Now VK5BAO.

VK3JYBE—T. T. G. Foster, Now VK5GTM.

VK4PL—W. J. Smith, Deceased.

VK4RM—R. E. McAdam, Not renewed.

VK4VP—J. V. Willis, Now VK5VP.

VK4ZKB—K. E. Ballantyne, Not renewed.

VK4ZLQ—L. A. Davies, Transferred to N.S.W.

VK4ZTA—T. J. Adams, Now VK5AYA.

VK5ZET—R. A. Fletcher, Transferred to W.A.

VK5ZGT—R. J. Chamberlain, Not renewed.

VK5ZQ—B. G. Dow, Deceased.

VK5SO—P. W. Williams, Now VK5CW.

VK5XW—C. P. Sheldie, Deceased.

VK5ZGZ—L. A. France, Not renewed.

VK5ZJ—A. L. Jackson, Not renewed.

VK5ZAS/T—R. S. Schahinger, Now VK5VT/T.

VK5ZDO—R. J. Watson, Not renewed.

VK5ZP—L. C. Stephens, Now VK5ZFH.

VK5ZSL—D. W. Friend, Transferred to N.S.W.

VK5ZPP—C. P. Dreher, Not renewed.

VK5AQ—G. R. Crews, Not renewed.

VK5TK—K. F. Gosling, Transferred to N.S.W.

VK5TL—B. V. Bulman, Now VK5YL.

VK5ZBA—J. A. Cooper, Now VK5JC.





## VHF NOTES

(continued from page 21)

George advises the Eastern Zone (Gippsland) v.h.f. boys have spent the winter constructing some very nice solid state gear for both v.h.f. and u.h.f., and generally upgrading their stations. Stations in the zone are on the lookout for amateur 144.180 and below from 1800 onwards. Also during periods of intense 6 m opening look for Gippsland 2 m stations on 144.005 and 144.188 MHz. By next summer the Eastern Zone boys hope to have a 1 m station running. Watch "Wellend news" (SLP) 14 different stations will be active on 6 m from the Eastern Zone this season, and on 2 m you might care to look for any of these: VK4, 3ASV, SYBY, 3ZNR, 3AXV, 3ZQC, 3ZKX, 3ZB, 3ZD, 3ZL and 3ZM, while those experimenting on 42 m MHz are 3ZQC, 3ZXM, 3ASV, SYBL, 3ZR, 3DR, 3JAX and 3ZNB.

Thank you George for filling in the gaps in the VK3 activity and this will now give those interested in short skip contacts plenty of opportunities.

Colin VK4DK (formerly VK5ZKR) of Mt. Gambier advises the South East Radio Group will be manning a portable expedition to "The Bluff" on the south coast of South Australia for the New Year holiday week-end, operating on all bands from 80 metres through to 1000 MHz.i

The station will be using the Club call sign VK5SEH. Colin advises further information next month, and with the earlier publication of "A.R." for January, the information should get to readers ahead of the actual week-end involved.

Finally, the Festive Season draws near. I take this opportunity of wishing you all a very happy and prosperous Christmas and New Year period. May it always be a time of transceivers in your Christmas stockings. Many thanks to those who have helped these pages along during the year with notes and snippets of information. Please keep it coming. It's your page, let me hear from you.

Thought for the month: "A good many men still like to think of their wives as they do of their religion—admitted, but always there. That's all until next month." T.S. Eric VK5LP The Voice in the Hills.

## CONTEST CALENDAR

\*12th Dec., 1970 to 11th Jan., 1971: Ross A. Hull V.H.F. Memorial Contest.

13th/14th Feb.: John Moyle Memorial National Field Day Contest.

\* N.B.—The dates initially published in the Contest Calendar have been altered to those shown above.

## KITS

**PM IF STRIP** (ref. "A.R." June '70), \$6.20. Wired and tested. \$11.20.

**CPE455E CERAMIC FILTER**, optional for above, 18 KHz bandwidth, \$18.00.

**1W. CI AUDIO AMP.** (ref. "A.R." July '70), \$8.80. Wired and tested. \$11.40.

**VARACTOR MULTIPLIER KIT**, 144 to 432 MHz. diode not supplied. \$5.80.

**2N3632 TRANSISTOR** (unbranded). May be used as v.h.f. amp or varactor. \$7.00.

**P8035 RECTIFIER-FILTER KIT**, 25V d.c. max. 2A. max. \$3.75. Wred and tested. \$4.25.

**H6004 VOLTAGE REGULATOR**, 4.5-12.5V. d.c. reg. max. 0.2A. max. \$9.85. Wred and tested. \$11.80.

All prices include sales tax and postage.

## COMMELEC INDUSTRIES

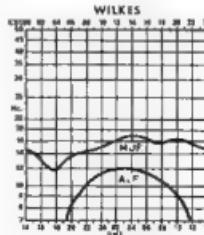
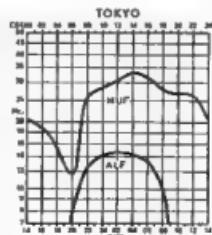
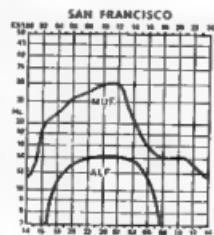
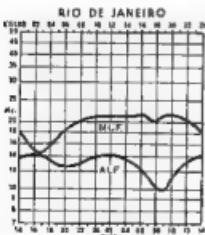
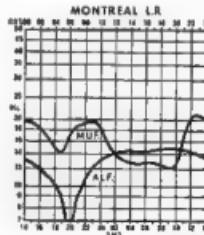
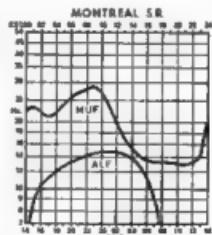
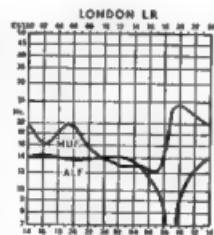
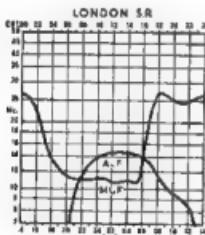
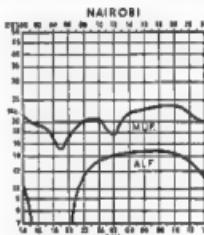
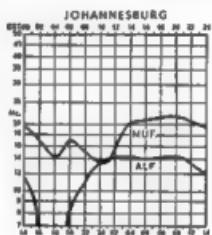
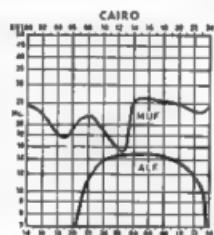
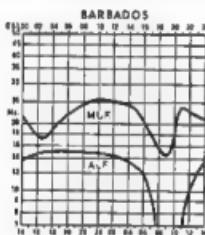
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## PREDICTION CHARTS FOR DECEMBER 1970

(Prediction Charts by courtesy of Ionospheric Prediction Service)



# Overseas Magazine Review

Compiled by Syd Clark, VK3ASC

## "BREAK-IN"

August 1970—

**Radio Apparatus.** ZL3ALC. This article is an explanation in the school-leaver of what is required of him should he wish to become a radio/t.v. serviceman.

**A Tale of Two VFOs.** ZL3AMU. Designed to give the usual one-handed transceiver two voices.

**Antenna Grids.** ZL3ALC. The meaning and measurement of this parameter.

**Circuit Accessories for the ZL3BDB Solid State Transceiver.** ZL3BDB. Vox, calibrator, three-watt audio output amplifier.

**An Experimental Panoramic Receiver.** ZL3AMU. A hand held to see where the others are on the band.

**Multipurpose Multivibrator.** ZL3ARP. Solid state versions of old friends.

## "CQ"

September 1970—

**Digital CQ and Meter Scatter Data Generators.** GM3MNQ. Part 1 of a two-part article on the subject of digital techniques of generating morse code. This article covers the basic building blocks used.

**AN DXpedition to Heard Island.** W7EZY, ex VK9WKR. Six DXpeditions seem to take place to palm fringed tropical islands. Here is one that went into the freezer.

**"CQ". Reviews the Drake TC-6 Six Meter Transceiving Converter.** WIAEF. Running 300 watt input to three 6J6s, this transverter is designed to be driven by a low power 16 MHz. exciter.

**Constructing Low-Loss Co-axial Transmission Lines.** VK4ZT. This article also appeared in "CQ".

**Using the Slide Rule to Determine L-C Circuits.** WA3GKH. A lesson in slip-stick working.

**Berry Tours Visit MARS Stations.** Don Dederer. The story of the tour of Senator Barry Goldwater's KU4A and VY4A.

**Motorizing Your Crank-up Tower.** KXHJ. A way of saving breath and cracked knuckles.

## "CQ TV"

August 1970—

**A Video Pin Sound Modulator.** by A. Maurer, HZ1PA.

**Television Camera Amplifier using the FET.** Mullard Ltd.

**Integrated Circuits.** A. W. Critchley. Using digital integrated circuits for t.v. pulse generation.

**A Low Power Transmitter.** GW3JGA/T

## "OHM"—The Oriental Ham Magazine

July 1970—

**Divided We Fall.** HS4ABD. The author considers that future allocations conferences could reduce native Amateurs' bands.

**RRA to Watch Spacecom.** Mest. Dealing with approach to H.A.R.T.S. by the Federal President of the R.W.L.A. (Michael J. O'Callaghan).

**Overseas Amateurs visited the J.A.R.L. Club Station JA3EXP at Expo '70, located in the San Francisco pavilion at the fair.**

**Power Supplies.** KR8TF. Reviews the various power supply circuits.

**Sea Rescue.** The follow up story to the rescue of Jens Jensen W4AMO/MM and wife Keiko.

## "QST"

August 1970—

**A Complete Solid State Portable for Forty Metres.** W3KTC. A portable/emergency c.w. station designed with certain requirements in mind. Here is a suitable station in a small package at minimum cost.

**QRP WIGER.** This is a second generation QRP "machine", designed and built in answer to many requests for a v.h.f. controlled version of the transceiver described in March 1970, QST.

**Multi-Watt Antennas.** KIRLM. The Mobile All Band Amateur V is the result of a search for high efficiency. We are sure this is a different antenna system.

**Short Antennas for the Lower Frequencies.** Part 1, W6JI. As operations on the lower frequencies have increased, this article looks at how to review the characteristics of short antennas and discusses means for tuning them.

**A Different Way To Get On Fifty MHz.** Bidash, WHDQ.

**Over 5 for Six.** WHEQKF. Describes an easily built stacked 50 MHz. array.

**Up Dates the SP-600.** WIKLK. Describes alterations he made to an SP-600 (Hammarlund) receiver to make it capable of receiving s.s.b. etc. The receiver is a later design than the AMER10, which was made in Australia during the war, some VFOs may be interested.

**The Operational Amplifier.** WOTCY. Part 1 describes a device which is in quite common use amongst the pros. Use in Amateur gear is increasing.

September 1970—

**A Solid State VOX.** WIKLK. Here is an easy to build circuit that is suitable as an onboard accessory, or it can be built into your next receiver.

**Short Antennas for Lower Frequencies.** Part 2, W6JI. Trap construction and adjustment.

**New Apparatus.** W1CP reviews that "VK-3ASC" Spider Quad Hub.

**Two Band Vertical for the Novice.** by WMMMP. An antenna which is ideal for the newcomer to Amateur Radio. Inexpensive and easy to construct.

**A QRP Console.** WICER. Combining low power s.w.r. meter with universal pi-section coupler. The speaker is also mounted in the console.

**U.H.F. Directional Couplers.** WRCQH and WZIMU. The ordinary "Monimatch" type instrument will not work satisfactorily at v.h.f. or u.h.f. Here are special designs for these bands.

**Automatic Amplifier Testing.** WSPHR. An electronic system for maintaining tank circuit controls.

**A Solid State Contest Receiver.** W1NHN. All you need to win is a good tx and a location with a four element beam on a 100 ft. mast on top of a mountain, plus a great deal of application.

**C.W. Break-in for the Collins 8-Line.** KOAZZ and W2WHN. The authors guarantee that this mod. will enhance the value of your Collins. The Operational Amplifier, WA1TCU Part 2. Some practical circuits.

## "RADIO COMMUNICATION"

August 1970—

**New Approach to V.H.F./U.H.F. Receivers.** Design, GSJPF. All solid state, trough lines, and other modern techniques.

**A New Receiver for Transistorized Receivers.** GSJGP. The title tells all.

**A Wide Range Crystal Calibrator using Integrated Circuits.** GSTDT. You'll have to read all of the words to know where the harmonics come from.

**Modifications to the Self Contained Linear Amplifier for 144 MHz.** GSJF.

**A 10 MHz. V.O.V.** GSJMNQ. Especially designed for those who do not like doublers 144 & 10 MHz. I.O.P.

**Technical Topics.** GSVA. In this issue of this monthly feature, Pat Hawker discusses methods of preventing interference with hi-fi equipment.

**Technical Topics.** GSVA. In this issue of this monthly feature, Pat Hawker discusses methods of preventing interference with hi-fi equipment.

**Narrow Band Frequency Modulation.** G3OGX. Using BA102 varicap. Circuit is simple and straightforward.

**Modifications for the H.R.O. P. Talbot. Case-Off r.f. stage circuit.**

**Mechanical Design for QRP V.H.F. Transmitter.** G3YUA. Guidance on the layout and construction of a transmitter.

August 1970—

**Transmitter Output Control Unit.** G4HLI. Incorporating aerial changer and switching, a.s.r. indicator and dummy load.

**Notes on the Trio JR-500, G3RPF.** Describes 1.8 MHz. mod. to this receiver.

**Antennas.** S.W. WILSON. Reprinted from article from "A.R." April 1970.

**Two Metre Transmitter in Kit Form.** G3ATX. P.C.B. design for a club project.

**Electrical Motors.** Code Generators.

**G3MNQ.** Considerations of circuit design for a sender.

## "THE INDIAN RADIO AMATEUR"

June 1970—

Perhaps some of the readers of "A.R." took particular note of an article stating that there were only about 450 Radio Amateurs in India. Considering the small number of Amateurs in that country, it is commendable that they manage to publish a regular magazine for the purpose of bringing news and notes to the Indian Radio Amateur and to print articles of local and overseas origin which appear to be of interest to the V.U.K.

## "THE AUSTRALIAN E.E.B."

August 1970 IV No. 8—

**Articles include:** C.D. Ignition (Part 1: Auto Ignition Interference); Pseudo High Voltage Modulator; The Radio Measuring Institute; Protection Resistor; Better Butter and Cake; Back to Front Voltage Regulator; Television Servicing (Part 2); FET Gate Diode Oscillator and Calibrator; Improved Fire Lighter; Amateur versus Ham. Review copy from the Australian E.E.B., P.O. Box 177, Sandy Bay, Tas.

## "VHF COMMUNICATIONS"

August 1970—

**A R.S.B. Transceiver with Silicon Transistor Complement.** DL3WAH. Part 3. Describes the 9-14 MHz. transmit-receive converter, the 14-144 MHz. transmit converter module with linear driver and 8 MHz. oscillator and low filter.

**Experiments with a Crystal Discriminator.** DJ4BG. Crystal discriminators are used extensively in commercial communications equipment.

**A Universal V.H.F.-U.H.F. Transmitter.** for A.M. and F.M. DL3WAH. Continued from edition two.

**Co-axial Low Pass Filters for V.H.F. and U.H.F.** DJ4QC. Many descriptions of the various types which can be made and how to make them. Constructional drawings are given.

**Electronically Stabilized Power Supply with B.C.-C. Coupling.** DJ3ZR.

**A Simple Rotary Co-axial Joint.** DC5OH. This joint is made from SC639 and PL259 parts with the addition of a few steel balls and a spring.

Review copy from Paul B. Jackson, 37 McKenna Rd., Bayview, N.S.W., 2104

"73"

August 1970—

**Mean That Mobile Right.** K4IPV. The right kind of mobile installation will result in bigger signals, better operator safety, and more fun in hammering on the road.

**Amateur Wattmeter for 83.5, K1CLL.** Components, lamp, brilliance, with standard 100 m.w. and 500 m.w. scales in the range from 150 metres through 450 MHz.

**Consume Console.** WB2FPH. How to increase the efficiency and enjoyment of your station by building a broadcast-style operating console.

**An Impedance Multiplier for the V.O.M.** by MD2GE. How to build a handy integrated-circuit device that turns your voltmeter into a V.T.V.M.

**Speaker Audio. Time Out for Quality.** by KG7HJ. Methods for improved audio matching, feed-back cancellation, and emitter followers.

**ATV. Getting a Better Picture.** WA8BJV. Upgrading systems by using better antennas, feeders, and switches.

**That Contest Craze.** VK5SS. A lot can happen between the thought and the deed.

**Log Periodic Designs for V.H.F.-U.H.F.** by WJDWQ. Spacing, dimensions and construction for log-periodic from 21 to 450 MHz.

**Ham Radio Chess.** W1EMW and WOBWM. Two notation systems for a pastime that's growing in popularity.

**V.H.F. A.M. Transmitter.** Brucker. Plans for a multi-band rig using low-cost transistors.

**Raising the Ambience.** WD4YDF. Problems of putting up one of those big ones.

**The 10-millimeter Goldstein.** Micromodularization that gives us, a.m. or e.w. on 20 through 160 meters.

**General Class Study Course.** Staff. Another chapter is a continuing technical series designed to help U.S. Hams up-grade their licences through improving their knowledge of theory.





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"QST," March 1959  
"Amateur Rad.," Dec. 1958.

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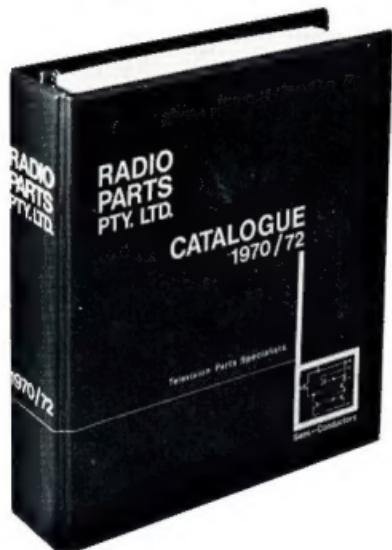
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